



VIBRATION SUPPRESSION OF A NON-LINEAR AXIALLY MOVING STRING BY BOUNDARY CONTROL

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1. INTRODUCTION

Axially moving string-like continua, such as threads, wires, magnetic tapes, belts, band-saws, chains and cables, have been subjects for study by researchers in recent years; see survey papers [1–3] for extensive lists of references. Researchers have derived and studied different linear and non-linear mathematical models which describe the dynamics of such systems; see, e.g., references [4–9]. Recently, the important problem of vibration suppression of axially moving string-like continua has received attention by researchers; see, e.g., references [10–15]. Most of the controllers, except that in reference [11], are designed on the basis of linear models of axially moving strings. Our goal in this note is to design a controller for a non-linear model of axially moving strings.

In this note, we consider the axially moving string in Figure 1. The string is pulled at a constant speed through two eyelets, which are distanced from each other by one unit of length. One of the eyelets is fixed and the other one can move freely in the direction of the Y-axis. A control input force, denoted by u in Figure 1, can be applied to the free-to-move eyelet transversally: i.e., in the direction of Y.

The dynamics of the string in Figure 1 can be represented by the following non-linear partial differential equation (see, e.g., references [1, 4, 11]):

$$y_{tt}(x,t) + 2avy_{xt}(x,t) = (1 - a^2v^2 + \frac{3}{2}by_x^2(x,t))y_{xx}(x,t),$$
(1a)

for all $x \in (0, 1)$ and $t \ge 0$. In equation (1a), $y(\cdot, \cdot) \in \mathbb{R}$ denotes the transversal displacement of the string, $y_x := \frac{\partial y}{\partial x}$, $y_{xx} := \frac{\partial^2 y}{\partial x^2}$, $y_{tt} := \frac{\partial^2 y}{\partial t^2}$, $y_{xt} := \frac{\partial^2 y}{\partial x} \frac{\partial t}{\partial t}$, a > 0 and b > 1 are constant real numbers, and v > 0 is proportional to the speed of the string through the eyelets. In realistic physical situations, av < 1.

The tension in the string represented by equation (1a) is *not* constant, and is given by

$$T(x, t) = 1 + \frac{1}{2}by_x^2(x, t),$$

for all $x \in [0, 1]$ and $t \ge 0$ (see reference [16]). With the tension *T*, we have the following boundary conditions:

$$y(0, t) = 0,$$
 $(1 - a^2v^2 + \frac{1}{2}by_x^2(1, t))y_x(1, t) = u(t),$ (1b, c)

for all $t \ge 0$. The boundary condition in equation (1b) states that the string is fixed at x = 0. The boundary condition in equation (1c) represents the balance of forces applied to the string at x = 1 in the direction of Y.

The initial displacement and velocity of the string are, respectively,

$$y(x, 0) = f(x), \qquad y_t(x, 0) = g(x),$$
 (1d)

for all $x \in (0, 1)$, where $y_t := \partial y / \partial t$. We assume that $f \in C^1[0, 1]$, and that at least one of the functions f and g is not identically zero over [0, 1].

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The control input u in equation (1c) is commonly known as the *boundary control*. In this note, we study the stabilization of the string in equation (1a) by u. More precisely, we study a u that results in $y(x, t) \rightarrow 0$ as $t \rightarrow \infty$ for all $x \in [0, 1]$. As a stabilizing control input, we propose

$$u(t) = -ky_t(1, t),$$
 (2)

for all $t \ge 0$, where k > 0 is a constant real number. With this choice of u, the boundary control is the negative feedback of the transversal velocity of the string at x = 1, with the gain k. It is known that fixed *linear* strings represented by equations (1), in which v = 0and b = 0, can be stabilized by the control law in equation (2); see, e.g., references [17–22]. Also, it is known that axially moving *linear* strings represented by equations (1), in which v > 0 and b = 0, can be stabilized by the control law in equation (2); see references [10, 13]. Roughly speaking, the boundary control in equation (2) provides a dissipative effect in linear strings, because it is of the form of negative velocity feedback. This is in accordance with the well known fact that the negative velocity feedback increases damping in most finite dimensional inertial systems, such as large flexible systems and robotic manipulators.

Our goal in this note is to show that the boundary control u in equation (2) stabilizes the non-linear axially moving non-linear string in equations (1), i.e., u results in $y(x, t) \rightarrow 0$ as $t \rightarrow \infty$ for all $x \in [0, 1]$. To the best of our knowledge, no such result exists.

2. STABILIZATION BY BOUNDARY CONTROL

Our plan to establish the stability of the non-linear string represented by equations (1) and (2) is as follows. We define an energy-like (Lyapunov) function of time for the string and denote it by $t \mapsto V(t)$. We show that V tends to zero exponentially.

We define the scalar-valued function V as

$$V(t) := E(t) + \gamma \int_0^1 \left[x y_t(x, t) y_x(x, t) + a v x y_x^2(x, t) \right] \mathrm{d}x, \tag{3}$$

for all $t \ge 0$, where $\gamma > 0$ is a constant real number,

$$E(t) := \frac{1}{2} \int_0^1 \left[y_t^2(x,t) + (1-a^2v^2)y_x^2(x,t) \right] \mathrm{d}x + \frac{b}{8} \int_0^1 y_x^4(x,t) \,\mathrm{d}x,\tag{4}$$



Figure 1. The string is pulled at a constant speed through two eyelets. The eyelet at x = 0 is fixed and the one at x = 1 can move freely in the direction of the Y-axis. The control input force $u(t) = -ky_t(1, t)$, for all $t \ge 0$, where k > 0 is a constant real number, is applied to the free-to-move eyelet in the direction of Y.

and $y(\cdot, \cdot)$ satisfies equations (1) and (2). From equations (3), (4) and (1d), we obtain

$$E(0) = \frac{1}{2} \int_0^1 \left[g^2(x) + (1 - a^2 v^2) f_x^2(x) \right] dx + \frac{b}{8} \int_0^1 f_x^4(x) dx,$$
 (5a)

$$V(0) = E(0) + \gamma \int_0^1 [xg(x)f_x(x) + avxf_x^2(x)] \,\mathrm{d}x,$$
(5b)

where $f_x(x) := df(x)/dx$. Since at least one of the functions f and g is not identically zero over [0, 1], we have E(0) > 0.

Now, we prove a property of V.

Lemma 2.1. Let γ in equation (3) satisfy

$$\gamma < \frac{1 - a^2 v^2}{1 + 2av}.\tag{6}$$

Then, the function V satisfies

$$0 \leqslant K_1 E(t) \leqslant V(t) \leqslant K_2 E(t), \tag{7}$$

for all $t \ge 0$, where $K_1 > 0$ and $K_2 > 0$ are constant real numbers, given by

$$K_1 = 1 - \frac{\gamma(1+2av)}{1-a^2v^2}, \qquad K_2 = 1 + \frac{\gamma(1+2av)}{1-a^2v^2}.$$
 (8a, b)

Proof. See Appendix A.

Remarks. (1) Since $(1 + 2av)/(1 - a^2v^2) > 1$ for all 0 < av < 1, it is clear that γ in inequality (6) is less than 1.

(2) Let γ satisfy inequality (6). Then, by inequality (7) and the fact that E(0) > 0, it is concluded that V(0) > 0.

Next, we substitute equation (2) into equation (1c) and rewrite the boundary conditions as

$$y(0, t) = 0,$$
 $y_x(1, t) = -\frac{ky_t(1, t)}{1 - a^2v^2 + \frac{1}{2}by_x^2(1, t)},$ (9a, b)

for all $t \ge 0$. We now prove some identities for the functions satisfying equations (9).

Lemma 2.2. let $y(\cdot, \cdot)$ satisfy the boundary conditions in equations (9). Then,

$$2\int_{0}^{1} y_{xt}y_{t} \, \mathrm{d}x = y_{t}^{2}(1, t), \qquad \int_{0}^{1} \left(y_{xx}y_{t} + y_{xt}y_{x} \right) \, \mathrm{d}x = -\frac{ky_{t}^{2}(1, t)}{1 - a^{2}v^{2} + \frac{1}{2}by_{x}^{2}(1, t)}, \quad (10a, b)$$

$$\int_{0}^{1} (3y_{xx}y_{x}^{2}y_{t} + y_{x}^{3}y_{xt}) \,\mathrm{d}x = -\frac{k^{3}y_{t}^{4}(1,t)}{[1 - a^{2}v^{2} + \frac{1}{2}by_{x}^{2}(1,t)]^{3}},\tag{10c}$$

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$$\int_{0}^{1} x y_{xt} y_{t} \, \mathrm{d}x = \frac{1}{2} y_{t}^{2}(1, t) - \frac{1}{2} \int_{0}^{1} y_{t}^{2} \, \mathrm{d}x, \qquad (10d)$$

$$\int_{0}^{1} x y_{xx} y_{x} \, \mathrm{d}x = \frac{k^{2} y_{i}^{2}(1, t)}{2[1 - a^{2} v^{2} + \frac{1}{2} b y_{x}^{2}(1, t)]^{2}} - \frac{1}{2} \int_{0}^{1} y_{x}^{2} \, \mathrm{d}x, \tag{10e}$$

$$\int_{0}^{1} x y_{xx} y_{x}^{3} dx = \frac{k^{4} y_{t}^{4}(1, t)}{4[1 - a^{2} v^{2} + \frac{1}{2} b y_{x}^{2}(1, t)]^{4}} - \frac{1}{4} \int_{0}^{1} y_{x}^{4} dx,$$
(10f)

for all $t \ge 0$.

Proof. See Appendix A.

Next, we compute the time derivative of the function E.

Lemma 2.3. The time derivative of the function E in equation (4), along the solution of the system (1a), (1c), and (9) (equivalently, the system (1) and (2)) satisfies

$$\dot{E}(t) = -avy_t^2(1,t) - \frac{k(1-a^2v^2)y_t^2(1,t)}{1-a^2v^2 + \frac{1}{2}by_x^2(1,t)} - \frac{k^3by_t^4(1,t)}{2[1-a^2v^2 + \frac{1}{2}by_x^2(1,t)]^3} \le 0, \quad (11)$$

for all $t \ge 0$.

Proof. See Appendix A.

Using the preliminary results obtained thus far, we next prove that the functions V and E tend to zero exponentially.

Theorem 2.4. Let γ in equation (3) satisfy

$$\gamma < \min\left\{\frac{1 - a^2 v^2}{1 + 2av}, 2av, \frac{4(1 - a^2 v^2)}{3k}\right\}.$$
(12)

Then, the functions V and E, along the solution of the system (1a), (1c) and (9) (equivalently, the system (1) and (2)) satisfy

$$0 \leq V(t) \leq V(0) e^{-\gamma t/K_2}, \quad 0 \leq E(t) \leq \frac{V(0)}{K_1} e^{-\gamma t/K_2},$$
 (13a, b)

for all $t \ge 0$, where K_1 and K_2 are given in equations (8).

Proof. From equation (3), we obtain

$$\dot{V}(t) = \dot{E}(t) + \gamma \int_0^1 \left(x y_{it} y_x + x y_t y_{xt} + 2a v x y_{xt} y_x \right) dx,$$
(14)

for all $t \ge 0$. Substituting y_{tt} from equation (1a) into equation (14), we obtain

$$\dot{V}(t) = \dot{E}(t) + \gamma \int_0^1 \left[x y_{xt} y_t + (1 - a^2 v^2) x y_{xx} y_x + \frac{3}{2} b x y_{xx} y_x^3 \right] \mathrm{d}x, \tag{15}$$

for all $t \ge 0$. Substituting equations (11), (10d), (10e) and (10f) into equation (15), we obtain

$$\dot{V}(t) \leqslant -\gamma E(t) - F(t), \tag{16}$$

for all $t \ge 0$, where

$$F(t) \coloneqq \left(av - \frac{\gamma}{2}\right) y_t^2(1, t) + \left(1 - \frac{\gamma k}{2(1 - a^2v^2)}\right) \frac{k(1 - a^2v^2)y_t^2(1, t)}{1 - a^2v^2 + \frac{1}{2}by_x^2(1, t)} \\ + \left(1 - \frac{3\gamma k}{4(1 - a^2v^2)}\right) \frac{k^3 b y_t^4(1, t)}{2[1 - a^2v^2 + \frac{1}{2}by_x^2(1, t)]^3}.$$
(17)

From inequality (12), we have

$$\gamma < \min\left\{2av, \frac{4(1-a^2v^2)}{3k}\right\},\tag{18}$$

by which we conclude that $F(t) \ge 0$ for all $t \ge 0$. Using the non-negativeness of F in inequality (16), we obtain

$$\dot{V}(t) \leqslant -\gamma E(t),\tag{19}$$

for all $t \ge 0$. Also, from inequality (12), we conclude that inequality (6) and hence inequality (7), hold. Using inequality (7) in inequality (19), we obtain the differential inequality

$$\dot{V}(t) \leqslant -\frac{\gamma}{K_2} V(t), \tag{20}$$

for all $t \ge 0$, with the initial condition V(0) given in equation (5b). By a comparison theorem given in references [23, p. 29] or [24, p. 30], we conclude that V in inequality (20) satisfies $V(t) \le V(0) e^{-\gamma t/K_2}$ for all $t \ge 0$. Note that, by inequality (7), we have $V(t) \ge 0$ for all $t \ge 0$. Thus, inequality (13a) holds. By inequalities (7) and (13a), we conclude that inequality (13b) holds.

Finally, we show that the boundary control u in equation (2) stabilizes the non-linear string in equations (1).

Corollary 2.5. The solution of the system (1a), (1c) and (9) (equivalently, the system (1) and (2)), $y(x, t) \rightarrow 0$ as $t \rightarrow \infty$ for all $x \in [0, 1]$.

Proof. For the system (1a), (1c) and (9), we choose the Lyapunov function V in equation (3), and let γ in equation (3) satisfy inequality (12). Then, by Theorem 2.4, the function E tends to zero exponentially. From equation (4), we conclude that $y_x(x, t) \rightarrow 0$ as $t \rightarrow \infty$ for all $x \in [0, 1]$. Since y(0, t) = 0 for all $t \ge 0$, we conclude that $y(x, t) \rightarrow 0$ as $t \rightarrow \infty$, for all $x \in [0, 1]$.

3. CONCLUSIONS

In this note, we have proved that the non-linear axially moving string represented by equations (1) can be stabilized by the linear boundary control in equation (2). The boundary control is the negative feedback of the transversal velocity of the string at one end.

REFERENCES

1. S. ABRATE 1992 Mechanism and Machine Theory 27, 645-659. Vibration of belts and belt drives.

LETTERS TO THE EDITOR

- 2. C. D. MOTE, JR. 1972 *The Shock and Vibration Digest* **4**, 2–11. Dynamic stability of axially moving materials.
- 3. J. A. WICKERT and C. D. MOTE, JR. 1988 *The Shock and Vibration Digest* **20**(5), 3–13. Current research on the vibration and stability of axially-moving materials.
- 4. C. D. MOTE, JR. 1966 *Journal of Applied Mechanics* 33, 463–464. On the nonlinear oscillation of an axially moving string.
- 5. M. PAKDEMIRLI, A. G. ULSOY and A. CERANOGLU 1994 *Journal of Sound and Vibration* 169, 179–196. Transverse vibration of an axially accelerating string.
- 6. J. A. WICKERT 1993 Journal of Sound and Vibration 160, 455–463. Analysis of self-excited longitudinal vibration of a moving tape.
- 7. J. A. WICKERT 1993 Journal of Vibration and Acoustics 115, 145–151. Free linear vibration of self-pressurized foil bearings.
- 8. J. A. WICKERT and C. D. MOTE, JR. 1990 Journal of Applied Mechanics 57, 738–744. Classical vibration analysis of axially moving continua.
- 9. W. D. ZHU and C. D. MOTE, JR. 1995 *Journal of Applied Mechanics* 62, 873–879. Propagation of boundary disturbances in an axially moving strip in contact with rigid and flexible constraints.
- 10. C. H. CHUNG and C. A. TAN 1995 *Journal of Vibration and Acoustics* 117, 49–55. Active vibration control of the axially moving string by wave cancellation.
- 11. R.-F. FUNG and C.-C. LIAO 1995 International Journal of Mechanical Sciences 37, 985–993. Application of variable structure control in the nonlinear string system.
- 12. A. GALIP ULSOY 1984 Journal of Dynamic Systems, Measurement, and Control 106, 6–14. Vibration control in rotating or translating elastic systems.
- 13. S.-Y. LEE and C. D. MOTE, JR. 1996 *Journal of Dynamic Systems, Measurement, and Control* 118, 66–74. Vibration control of an axially moving string by boundary control.
- 14. B. YANG and C. D. MOTE, JR. 1991 *Journal of Applied Mechanics* 58, 189–196. Active vibration control of the axially moving string in the S domain.
- 15. S. YING and C. A. TAN 1996 Journal of Vibration and Acoustics 118, 306–312. Active vibration control of the axially moving string using space feedforward and feedback controllers.
- 16. G. S. S. MURTHY and B. S. RAMAKRISHNA 1965 Journal of the Acoustical Society of America 38, 461–471. Nonlinear character of resonance in stretched strings.
- 17. G. CHEN 1979 Journal de Mathématiques Pures et Appliquées 58, 249–273. Energy decay estimates and exact boundary value controllability for the wave equation in a bounded domain.
- 18. G. CHEN 1981 SIAM Journal of Control and Optimization 19, 106–113. A note on boundary stabilization of the wave equation.
- V. KOMONIK and E. ZUAZUA 1990 Journal de Mathématiques Pures et Appliquées 69, 33–54. A direct method for the boundary stabilization of the wave equation.
- 20. J. LAGNESE 1983 *Journal of Differential Equations* 50, 163–182. Decay of solutions of wave equations in a bounded region with boundary dissipation.
- 21. J. E. LAGNESE 1988 *SIAM Journal of Control and Optimization* **26**, 1250–1256. Note on boundary stabilization of wave equations.
- 22. J. QUINN and D. L. RUSSELL 1977 *Proceedings of the Royal Society of Edinburgh* **77A**, 97–127. Asymptotic stability and energy decay rates for solutions of hyperbolic equations with boundary damping.
- 23. G. BIRKHOff and G. C. ROTA 1989 Ordinary Differential Equations. New York: John Wiley; fourth edition.
- 24. V. LAKSHMIKANTHAM, S. LEELA and A. A. MARTYNYUK 1989 Stability Analysis of Nonlinear Systems. New York: Marcel Dekker.

APPENDIX A: PROOFS

A.1. Proof of Lemma 2.1.

For the integral terms in equation (3), the coefficient of which is γ , we have (the argument (x, t) of the functions is deleted)

$$\int_{0}^{1} xy_{t}y_{x} \, \mathrm{d}x \leqslant \int_{0}^{1} x|y_{t}| \|y_{x}| \, \mathrm{d}x \leqslant \frac{1}{2} \int_{0}^{1} y_{t}^{2} \, \mathrm{d}x + \frac{1}{2} \int_{0}^{1} y_{x}^{2} \, \mathrm{d}x, \qquad \int_{0}^{1} avxy_{x}^{2} \, \mathrm{d}x \leqslant av \int_{0}^{1} y_{x}^{2} \, \mathrm{d}x,$$
(A1a, b)

for all $t \ge 0$. Thus,

$$\int_{0}^{1} (xy_{t}y_{x} + avxy_{x}^{2}) \, \mathrm{d}x \leq \frac{1}{2} \int_{0}^{1} y_{t}^{2} \, \mathrm{d}x + \frac{1 + 2av}{2(1 - a^{2}v^{2})} \int_{0}^{1} (1 - a^{2}v^{2})y_{x}^{2} \, \mathrm{d}x, \tag{A2}$$

for all $t \ge 0$. Since

$$\frac{1+2av}{1-a^2v^2} \ge 1,\tag{A3}$$

for all 0 < av < 1, we conclude that

$$\int_{0}^{1} \left(xy_{t}y_{x} + avxy_{x}^{2} \right) \mathrm{d}x \leqslant \frac{1 + 2av}{1 - a^{2}v^{2}} \left(\frac{1}{2} \int_{0}^{1} \left[y_{t}^{2} + (1 - a^{2}v^{2})y_{x}^{2} \right] \mathrm{d}x \right) \leqslant \frac{1 + 2av}{1 - a^{2}v^{2}} E(t), \quad (A4a)$$

for all $t \ge 0$. Similarly, we obtain

$$\int_{0}^{1} (xy_{t}y_{x} + avxy_{x}^{2}) \,\mathrm{d}x \ge -\frac{1+2av}{1-a^{2}v^{2}}E(t), \tag{A4b}$$

for all $t \ge 0$. Using equations (A4) in equation (3), we obtain equation (7).

A.2. Proof of Lemma 2.2.

From equation (9a), we have $y_t(0, t) = 0$ for all $t \ge 0$. Thus, we obtain

$$2\int_{0}^{1} y_{xt}y_{t} \, \mathrm{d}x = \int_{0}^{1} (y_{t}^{2})_{x} \, \mathrm{d}x = y_{t}^{2}(1, t), \tag{A5}$$

for all $t \ge 0$. That is, equation (10a) holds.

Having $y_t(0, t) = 0$ for all $t \ge 0$, we next obtain

$$\int_{0}^{1} (y_{xx}y_{t} + y_{xt}y_{x}) dx = \int_{0}^{1} (y_{x}y_{t})_{x} dx = y_{x}(1, t)y_{t}(1, t),$$
(A6)

for all $y \ge 0$. Using equation (9b) in equation (A6), we obtain equation (10b).

Having $y_t(0, t) = 0$ for all $t \ge 0$, we next obtain

$$\int_{0}^{1} (3y_{xx}y_{x}^{2}y_{t} + y_{x}^{3}y_{xt}) \, \mathrm{d}x = \int_{0}^{1} (y_{x}^{3}y_{t})_{x} \, \mathrm{d}x = y_{x}^{3}(1,t)y_{t}(1,t), \tag{A7}$$

for all $t \ge 0$. Using equation (9b) in equation (A7), we obtain equation (10c).

Next, we write

$$\int_{0}^{1} x y_{xt} y_{t} \, \mathrm{d}x = \frac{1}{2} \int_{0}^{1} (x y_{t}^{2})_{x} \, \mathrm{d}x - \frac{1}{2} \int_{0}^{1} y_{t}^{2} \, \mathrm{d}x, \tag{A8}$$

for all $t \ge 0$. Thus, equation (10d) follows.

Next, we write

$$\int_{0}^{1} x y_{xx} y_{x} \, \mathrm{d}x = \frac{1}{2} \int_{0}^{1} (x y_{x}^{2})_{x} \, \mathrm{d}x - \frac{1}{2} \int_{0}^{1} y_{x}^{2} \, \mathrm{d}x = \frac{1}{2} y_{x}^{2} (1, t) - \frac{1}{2} \int_{0}^{1} y_{x}^{2} \, \mathrm{d}x, \tag{A9}$$

for all $t \ge 0$. Using equation (9b) in equation (A9), we obtain equation (10e). Finally, we write

 $\int_{0}^{1} xy_{xx}y_{x}^{3} dx = \frac{1}{4} \int_{0}^{1} (xy_{x}^{4})_{x} dx - \frac{1}{4} \int_{0}^{1} y_{x}^{4} dx = \frac{1}{4}y_{x}^{4}(1, t) - \frac{1}{4} \int_{0}^{1} y_{x}^{4} dx,$ (A10)

for all $t \ge 0$. Using equation (9b) in equation (A10), we obtain equation (10f).

A.3. Proof of Lemma 2.3.

From equation (4), we obtain

$$\dot{E}(t) = \int_0^1 \left[y_{tt} y_t + (1 - a^2 v^2) y_{xt} y_x \right] \mathrm{d}x + \frac{b}{2} \int_0^1 y_{xt} y_x^3 \, \mathrm{d}x, \tag{A11}$$

for all $t \ge 0$. Substituting y_{tt} from equation (1a) into equation (A11), we obtain

$$\dot{E}(t) = -2av \int_{0}^{1} y_{xt}y_{t} \, \mathrm{d}x + (1 - a^{2}v^{2}) \int_{0}^{1} (y_{xx}y_{t} + y_{xt}y_{x}) \, \mathrm{d}x$$
$$+ \frac{b}{2} \int_{0}^{1} (3y_{xx}y_{x}^{2}y_{t} + y_{x}^{3}y_{xt}) \, \mathrm{d}x, \qquad (A12)$$

for all $t \ge 0$. Using equations (10a), (10b) and (10c) in equation (A12), we obtain equation (11).